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1650

Original Cross Sections of Borrow Pit

44

H 719+51L A.E.O $\frac{7.8}{40.0}$ $\frac{8.1}{44.0}$ $\frac{9.0}{50.0}$ $\frac{9.1}{74.0}$ $\frac{8.1}{79.0}$ $\frac{8.0}{84.0}$ $\frac{6.3}{89.0}$ $\frac{6.1}{91.0}$ $\frac{7.2}{93.0}$ $\frac{7.6}{95.0}$ $\frac{12.1}{103.0}$ $\frac{13.1}{106.0}$ $\frac{14.4}{109.0}$ $\frac{14.3}{115.0}$ $\frac{13.0}{120.0}$ $\frac{10.5}{125.0}$

$\frac{8.9}{130.0}$ $\frac{7.0}{133.0}$ $\frac{6.3}{138.0}$ $\frac{7.0}{145.0}$ $\frac{9.6}{146.5}$

720 $\frac{7.8}{45.0}$ $\frac{9.1}{50.0}$ $\frac{9.0}{76.0}$ $\frac{9.1}{87.0}$ $\frac{6.6}{92.0}$ $\frac{6.9}{96.0}$ $\frac{9.8}{100.0}$ $\frac{12.0}{106.0}$ $\frac{13.9}{109.0}$ $\frac{14.3}{113.0}$ $\frac{14.1}{117.0}$ $\frac{11.6}{123.0}$ $\frac{9.6}{128.0}$ $\frac{5.8}{138.0}$ $\frac{5.8}{143.0}$ $\frac{7.2}{148.0}$

$\frac{8.9}{149.3}$

+50 $\frac{7.7}{42.0}$ $\frac{7.8}{46.0}$ $\frac{8.7}{57.0}$ $\frac{8.7}{76.0}$ $\frac{6.3}{80.0}$ $\frac{6.7}{93.0}$ $\frac{7.9}{99.0}$ $\frac{10.8}{105.0}$ $\frac{12.4}{109.0}$ $\frac{14.5}{113.0}$ $\frac{14.2}{117.0}$ $\frac{11.5}{123.0}$ $\frac{8.0}{138.0}$ $\frac{5.9}{141.0}$ $\frac{5.6}{150.0}$ $\frac{8.6}{152.1}$

721 $\frac{6.8}{44.0}$ $\frac{8.4}{57.0}$ $\frac{7.9}{75.0}$ $\frac{7.1}{78.0}$ $\frac{6.3}{83.0}$ $\frac{4.9}{93.0}$ $\frac{10.2}{104.0}$ $\frac{13.0}{110.0}$ $\frac{14.3}{113.0}$ $\frac{14.2}{117.0}$ $\frac{11.3}{125.0}$ $\frac{10.6}{132.0}$ $\frac{6.1}{139.0}$ $\frac{4.8}{146.0}$ $\frac{4.9}{152.6}$ $\frac{7.9}{154.9}$

1

H 721+50 $\frac{5.4}{44.0}$ $\frac{8.1}{50.0}$ $\frac{7.9}{73.0}$ $\frac{5.7}{80.0}$ $\frac{4.8}{88.0}$ $\frac{5.7}{96.0}$ $\frac{8.3}{102.0}$ $\frac{10.6}{107.0}$ $\frac{13.1}{113.0}$ $\frac{14.0}{116.0}$ $\frac{14.0}{119.0}$ $\frac{11.4}{125.0}$ $\frac{9.6}{131.0}$ $\frac{6.7}{139.0}$ $\frac{4.7}{146.0}$ $\frac{4.8}{154.0}$ $\frac{7.3}{157.0}$

722 $\frac{5.9}{46.0}$ $\frac{7.9}{50.0}$ $\frac{7.5}{73.0}$ $\frac{5.3}{80.0}$ $\frac{8.3}{88.0}$ $\frac{6.1}{100.0}$ $\frac{10.0}{108.0}$ $\frac{11.3}{111.0}$ $\frac{14.4}{116.0}$ $\frac{14.2}{119.0}$ $\frac{12.8}{123.0}$ $\frac{11.3}{126.0}$ $\frac{9.2}{131.0}$ $\frac{7.9}{137.0}$ $\frac{4.4}{149.0}$ $\frac{4.6}{158.0}$ $\frac{7.2}{160.4}$

+50 $\frac{4.1}{44.0}$ $\frac{7.6}{47.0}$ $\frac{5.3}{74.0}$ $\frac{4.3}{81.0}$ $\frac{3.6}{89.0}$ $\frac{4.0}{94.0}$ $\frac{8.0}{104.0}$ $\frac{9.5}{108.0}$ $\frac{12.5}{114.0}$ $\frac{14.5}{118.0}$ $\frac{14.2}{120.0}$ $\frac{13.0}{124.0}$ $\frac{10.6}{130.0}$ $\frac{8.6}{137.0}$ $\frac{5.9}{145.0}$ $\frac{4.4}{150.0}$ $\frac{5.8}{161.0}$ $\frac{7.7}{163.2}$

723 $\frac{6.8}{45.0}$ $\frac{8.0}{48.0}$ $\frac{7.9}{74.0}$ $\frac{4.4}{82.0}$ $\frac{4.0}{93.0}$ $\frac{10.0}{109.0}$ $\frac{14.3}{114.0}$ $\frac{14.5}{118.0}$ $\frac{14.4}{124.0}$ $\frac{11.8}{127.0}$ $\frac{8.6}{130.0}$ $\frac{5.8}{141.0}$ $\frac{4.9}{155.0}$ $\frac{4.6}{162.0}$ $\frac{8.1}{166.0}$

H 723+50 $\frac{6.9}{44.0}$ $\frac{7.9}{49.0}$ $\frac{7.5}{74.0}$ $\frac{5.4}{80.0}$ $\frac{4.4}{86.0}$ $\frac{4.2}{94.0}$ $\frac{9.1}{105.0}$ $\frac{10.9}{112.0}$ $\frac{13.6}{116.0}$ $\frac{15.0}{119.0}$ $\frac{14.6}{130.0}$ $\frac{11.2}{140.0}$ $\frac{6.6}{145.0}$ $\frac{4.5}{152.0}$ $\frac{4.3}{161.0}$ $\frac{7.7}{165.0}$ $\frac{8.0}{168.0}$

724 $\frac{6.9}{44.0}$ $\frac{7.8}{48.0}$ $\frac{7.2}{74.0}$ $\frac{4.9}{82.0}$ $\frac{4.2}{89.0}$ $\frac{4.7}{97.0}$ $\frac{7.8}{104.0}$ $\frac{10.2}{112.0}$ $\frac{11.2}{114.0}$ $\frac{14.1}{117.0}$ $\frac{14.9}{120.0}$ $\frac{14.4}{123.0}$ $\frac{11.5}{125.0}$ $\frac{9.1}{136.0}$ $\frac{6.6}{145.0}$ $\frac{5.6}{154.0}$

$\frac{4.6}{153.0}$ $\frac{4.8}{159.0}$ $\frac{4.6}{166.0}$ $\frac{7.3}{169.0}$ $\frac{7.7}{171.6}$

+50 $\frac{6.8}{47.0}$ $\frac{7.9}{51.0}$ $\frac{7.6}{72.0}$ $\frac{5.6}{79.0}$ $\frac{4.9}{84.0}$ $\frac{4.5}{97.0}$ $\frac{8.3}{106.0}$ $\frac{10.0}{112.0}$ $\frac{10.8}{114.0}$ $\frac{10.9}{118.0}$ $\frac{14.2}{121.0}$ $\frac{14.4}{124.0}$ $\frac{11.4}{130.0}$ $\frac{9.5}{135.0}$ $\frac{5.8}{149.0}$

$\frac{4.0}{158.0}$ $\frac{4.3}{170.0}$ $\frac{7.4}{174.4}$

726 $\frac{4.2}{48.0}$ $\frac{7.5}{51.0}$ $\frac{7.7}{73.0}$ $\frac{5.2}{80.0}$ $\frac{5.8}{89}$ $\frac{4.1}{97.0}$ $\frac{7.2}{105.0}$ $\frac{9.0}{109.0}$ $\frac{11.5}{117.0}$ $\frac{13.5}{121.0}$ $\frac{13.5}{128.0}$ $\frac{11.6}{132.0}$ $\frac{10.0}{137.0}$ $\frac{6.8}{147.0}$ $\frac{4.8}{154.0}$ $\frac{9.8}{162.0}$

$\frac{4.0}{158.0}$ $\frac{6.5}{176.0}$

1653

Original Cross Sections of Borrow Pit

H 725+50 $\frac{8.0}{50.0}$ $\frac{7.7}{74.0}$ $\frac{6.0}{80.0}$ $\frac{4.5}{95.0}$ $\frac{4.6}{100.0}$ $\frac{9.6}{114.0}$ $\frac{11.3}{118.0}$ $\frac{14.5}{124.0}$ $\frac{14.1}{128.0}$ $\frac{11.2}{135.0}$ $\frac{6.0}{151.0}$ $\frac{3.8}{160.0}$ $\frac{3.7}{166.0}$ $\frac{4.2}{173.0}$

$\frac{5.9}{177.1}$

726 $\frac{13.8}{30.0}$ $\frac{10.1}{36.0}$ $\frac{6.1}{42.0}$ $\frac{8.5}{50.0}$ $\frac{8.4}{59.0}$ $\frac{7.8}{78.0}$ $\frac{7.7}{92.0}$ $\frac{5.5}{96.0}$ $\frac{5.0}{100.0}$ $\frac{10.4}{114.0}$ $\frac{12.6}{120.0}$ $\frac{14.7}{124.0}$ $\frac{14.5}{129.0}$ $\frac{10.9}{138.0}$

$\frac{5.5}{157.0}$ $\frac{3.9}{167.0}$ $\frac{3.4}{173.0}$ $\frac{5.6}{177.0}$ $\frac{7.2}{178.5}$

+50 $\frac{13.8}{33.0}$ $\frac{10.1}{36.0}$ $\frac{8.2}{42.0}$ $\frac{8.4}{60.0}$ $\frac{8.3}{89.0}$ $\frac{6.7}{94.0}$ $\frac{5.8}{100.0}$ $\frac{6.2}{105.0}$ $\frac{11.6}{115.0}$ $\frac{12.6}{121.0}$ $\frac{14.4}{125.0}$ $\frac{14.3}{130.0}$ $\frac{10.7}{134.0}$ $\frac{10.6}{140.0}$ $\frac{9.1}{150.0}$

$\frac{5.4}{158.0}$ $\frac{4.2}{168.0}$ $\frac{4.7}{177.0}$ $\frac{7.7}{180.0}$

727 $\frac{13.7}{33.0}$ $\frac{11.6}{37.0}$ $\frac{8.1}{43.0}$ $\frac{9.2}{45.0}$ $\frac{8.5}{60.0}$ $\frac{8.2}{89.0}$ $\frac{6.1}{96.0}$ $\frac{5.7}{100.0}$ $\frac{5.9}{103.0}$ $\frac{10.7}{115.0}$ $\frac{12.2}{121.0}$ $\frac{14.6}{127.0}$ $\frac{14.3}{131.0}$ $\frac{11.1}{140.0}$ $\frac{7.1}{154.0}$

$\frac{5.7}{159.0}$ $\frac{4.3}{169.0}$ $\frac{5.2}{176.0}$ $\frac{9.1}{181.8}$

H 727+50 $\frac{13.7}{33.0}$ $\frac{11.9}{37.0}$ $\frac{8.1}{41.0}$ $\frac{8.2}{45.0}$ $\frac{8.1}{54.0}$ $\frac{8.4}{61.0}$ $\frac{8.1}{92.0}$ $\frac{6.3}{100.0}$ $\frac{6.3}{104.0}$ $\frac{10.5}{116.0}$ $\frac{12.9}{123.0}$ $\frac{14.6}{127.0}$ $\frac{14.3}{132.0}$ $\frac{11.4}{141.0}$ $\frac{7.5}{154.0}$

$\frac{5.8}{160.0}$ $\frac{4.6}{169.0}$ $\frac{5.3}{176.0}$ $\frac{5.6}{179.0}$ $\frac{8.7}{182.4}$

728 $\frac{13.6}{33.0}$ $\frac{11.7}{37.0}$ $\frac{8.0}{41.0}$ $\frac{7.8}{51.0}$ $\frac{8.3}{62.0}$ $\frac{8.2}{73.0}$ $\frac{7.3}{76.0}$ $\frac{6.7}{97.0}$ $\frac{6.1}{100.0}$ $\frac{6.7}{106.0}$ $\frac{10.3}{117.0}$ $\frac{13.2}{125.0}$ $\frac{14.7}{129.0}$ $\frac{14.6}{133.0}$

$\frac{13.2}{138.0}$ $\frac{9.4}{149.0}$ $\frac{7.4}{155.0}$ $\frac{6.3}{158.0}$ $\frac{4.8}{165.0}$ $\frac{4.6}{171.0}$ $\frac{5.1}{176.0}$ $\frac{5.8}{181.0}$ $\frac{8.6}{183.8}$

+50 $\frac{11.5}{25.0}$ $\frac{8.1}{40.0}$ $\frac{7.5}{51.0}$ $\frac{7.8}{63.0}$ $\frac{7.9}{90.0}$ $\frac{6.0}{96.0}$ $\frac{5.3}{100.0}$ $\frac{5.6}{107.0}$ $\frac{7.2}{112.0}$ $\frac{10.5}{118.0}$ $\frac{13.6}{124.0}$ $\frac{15.0}{128.0}$ $\frac{14.4}{134.0}$ $\frac{12.4}{140.0}$ $\frac{7.6}{155.0}$

$\frac{6.0}{161.0}$ $\frac{4.9}{171.0}$ $\frac{5.4}{176.0}$ $\frac{7.2}{181.0}$ $\frac{8.9}{185.2}$

729 $\frac{11.3}{37.0}$ $\frac{8.1}{40.0}$ $\frac{7.8}{51.0}$ $\frac{8.3}{63.0}$ $\frac{7.7}{93.0}$ $\frac{6.7}{96.0}$ $\frac{5.8}{100.0}$ $\frac{6.6}{106.0}$ $\frac{11.0}{118.0}$ $\frac{13.3}{124.0}$ $\frac{16.1}{129.0}$ $\frac{14.9}{135.1}$ $\frac{13.6}{140.0}$ $\frac{11.3}{146.0}$ $\frac{7.5}{158.0}$

$\frac{5.9}{164.0}$ $\frac{5.0}{171.0}$ $\frac{5.8}{172.0}$ $\frac{7.2}{182.0}$ $\frac{9.4}{186.6}$

1655

H 729+50 14.0/31.0 11.4/37.0 8.2/41.0 8.4/63.0 7.7/94.0 5.8/100.0 5.6/105.0 6.7/109.0 10.6/120.0 13.1/126.0 15.1/131.0 14.8/137.0 13.5/142.0 11.6/147.0 7.2/167.0

5.0/170.0 4.8/175.0 5.7/180.0 7.3/184.0 9.2/187.4

730 14.2/31.0 11.7/37.0 8.6/41.0 8.7/49.0 8.6/63.0 8.3/92.0 5.7/100.0 5.6/105.0 6.6/111.0 10.2/120.0 13.3/128.0 14.9/133.0 14.6/137.0 12.1/145.0 8.8/156.0

6.3/164.0 5.0/171.0 4.9/176.0 5.8/183.0 6.9/187.0 8.0/188.5

+50 14.2/33.0 12.1/38.0 8.3/43.0 8.7/46.0 9.3/57.0 8.3/92.0 6.7/97.0 6.1/105.0 6.6/112.0 11.1/121.0 13.9/128.0 14.7/134.0 14.8/137.0 11.7/147.0 7.7/160.0

5.0/170.0 4.6/177.0 5.1/183.0 7.2/188.0 8.9/190.7

731 14.9/31.0 12.2/38.0 8.5/42.0 7.9/47.0 9.1/58.0 8.9/92.0 7.5/98.0 5.9/106.0 6.7/110.0 11.8/122.0 13.5/130.0 14.7/135.0 14.6/139.0 11.4/151.0 7.5/163.0

4.6/172.0 4.1/179.0 5.0/185.0 6.3/188.0 8.8/192.9

1656

H 731+50 $\frac{14.9}{31.0}$ $\frac{12.6}{38.0}$ $\frac{8.0}{45.0}$ $\frac{7.8}{50.0}$ $\frac{8.1}{54.0}$ $\frac{8.9}{58.0}$ $\frac{8.9}{93.0}$ $\frac{6.5}{100.0}$ $\frac{6.2}{107.0}$ $\frac{6.8}{110.0}$ $\frac{11.5}{121.0}$ $\frac{13.8}{130.0}$ $\frac{15.2}{137.0}$ $\frac{14.8}{141.0}$ $\frac{12.4}{149.0}$

$\frac{9.2}{159.0}$ $\frac{6.5}{168.0}$ $\frac{4.6}{176.0}$ $\frac{4.2}{181.0}$ $\frac{4.7}{186.0}$ $\frac{6.7}{190.0}$ $\frac{8.1}{192.0}$ $\frac{8.1}{194.8}$

732 $\frac{15.0}{29.0}$ $\frac{14.2}{32.0}$ $\frac{11.2}{38.0}$ $\frac{7.4}{46.0}$ $\frac{8.2}{54.0}$ $\frac{9.1}{59.0}$ $\frac{8.6}{94.0}$ $\frac{6.7}{100.0}$ $\frac{6.2}{107.0}$ $\frac{6.8}{112.0}$ $\frac{9.9}{118.0}$ $\frac{11.5}{122.0}$ $\frac{13.9}{131.0}$ $\frac{15.3}{136.0}$ $\frac{14.7}{142.0}$

$\frac{11.8}{152.0}$ $\frac{9.3}{160.0}$ $\frac{6.5}{169.0}$ $\frac{4.3}{176.0}$ $\frac{4.7}{183.0}$ $\frac{5.7}{188.0}$ $\frac{6.6}{191.0}$ $\frac{8.1}{195.0}$ $\frac{7.1}{197.0}$

+50 $\frac{15.0}{31.0}$ $\frac{13.6}{35.0}$ $\frac{8.3}{43.0}$ $\frac{7.5}{50.0}$ $\frac{9.1}{57.0}$ $\frac{9.4}{60.0}$ $\frac{9.1}{74.0}$ $\frac{6.8}{100.0}$ $\frac{6.5}{107.0}$ $\frac{6.9}{112.0}$ $\frac{11.3}{123.0}$ $\frac{12.2}{131.0}$ $\frac{15.1}{137.0}$ $\frac{14.8}{144.0}$ $\frac{11.2}{154.0}$ $\frac{8.9}{164.0}$

$\frac{6.0}{172.0}$ $\frac{4.8}{176.0}$ $\frac{4.2}{184.0}$ $\frac{5.3}{191.0}$ $\frac{8.1}{195.0}$ $\frac{8.2}{199.2}$

733 $\frac{14.7}{33.0}$ $\frac{13.0}{38.0}$ $\frac{8.3}{43.0}$ $\frac{7.9}{54.0}$ $\frac{8.2}{62.0}$ $\frac{9.2}{63.0}$ $\frac{9.6}{73.0}$ $\frac{6.9}{100.0}$ $\frac{6.6}{104.0}$ $\frac{6.9}{114.0}$ $\frac{10.5}{120.0}$ $\frac{11.6}{124.0}$ $\frac{14.0}{134.0}$ $\frac{15.0}{138.0}$ $\frac{15.0}{142.0}$ $\frac{12.1}{151.0}$

$\frac{11.5}{155.0}$ $\frac{6.6}{171.0}$ $\frac{6.1}{172.0}$ $\frac{4.7}{177.0}$ $\frac{3.7}{184.0}$ $\frac{4.0}{189.0}$ $\frac{6.6}{193.0}$ $\frac{8.0}{197.0}$ $\frac{7.9}{201.4}$

1657

H733 450 $\frac{14.7}{31.0}$ $\frac{11.7}{39.0}$ $\frac{7.9}{43.0}$ $\frac{6.6}{47.0}$ $\frac{6.2}{55.0}$ $\frac{7.5}{62.3}$

734 $\frac{9.7}{35.0}$ $\frac{7.4}{42.0}$ $\frac{6.4}{44.0}$ $\frac{6.8}{49.0}$ $\frac{7.4}{58.0}$ $\frac{8.7}{64.0}$ $\frac{8.0}{96.0}$

450 $\frac{9.7}{41.0}$ $\frac{6.4}{41.6}$ $\frac{7.9}{49.0}$ $\frac{9.4}{65}$ $\frac{7.7}{97.0}$ $\frac{6.1}{100.0}$ $\frac{5.4}{106.0}$

735 $\frac{6.3}{47.0}$ $\frac{6.5}{56.0}$ $\frac{7.9}{67.0}$ $\frac{7.0}{100.0}$ $\frac{6.0}{102.0}$ $\frac{4.4}{109.0}$

$\frac{9.0}{64.0}$ $\frac{8.8}{94.0}$ $\frac{6.8}{100.0}$ $\frac{6.1}{108.0}$ $\frac{6.5}{114.0}$ $\frac{9.7}{121.0}$ $\frac{10.7}{125.0}$ $\frac{13.7}{136.0}$ $\frac{14.4}{139.0}$ $\frac{14.6}{143.0}$

$\frac{13.1}{149.0}$ $\frac{11.4}{157.0}$ $\frac{6.5}{172.0}$ $\frac{6.9}{175.0}$ $\frac{3.6}{181.0}$ $\frac{3.6}{186.0}$ $\frac{3.8}{189.0}$ $\frac{6.3}{194.0}$ $\frac{8.0}{198.0}$ $\frac{9.6}{203.8}$

$\frac{6.9}{100.0}$ $\frac{5.9}{104.0}$ $\frac{5.7}{110.0}$ $\frac{5.7}{114.0}$ $\frac{10.4}{125.0}$ $\frac{12.4}{134.0}$ $\frac{14.5}{139.0}$ $\frac{14.3}{144.0}$ $\frac{11.6}{153.0}$

$\frac{7.7}{166.0}$ $\frac{5.8}{177.0}$ $\frac{3.6}{180.0}$ $\frac{3.3}{187.0}$ $\frac{3.7}{191.0}$ $\frac{5.9}{195.0}$ $\frac{7.6}{200.0}$ $\frac{7.4}{205.9}$

$\frac{5.3}{114.0}$ $\frac{10.9}{126.0}$ $\frac{13.1}{134.0}$ $\frac{14.4}{139.0}$ $\frac{14.3}{143.0}$ $\frac{10.9}{153.0}$ $\frac{7.0}{167.0}$ $\frac{4.8}{178.0}$

$\frac{3.6}{181.0}$ $\frac{3.3}{187.0}$ $\frac{3.5}{192.0}$ $\frac{6.0}{196.0}$ $\frac{7.2}{200.0}$ $\frac{7.1}{208.2}$

$\frac{4.6}{115.0}$ $\frac{7.6}{127.0}$ $\frac{14.4}{139.0}$ $\frac{14.1}{144.0}$ $\frac{8.3}{164.0}$ $\frac{3.6}{180.0}$ $\frac{3.3}{189.0}$ $\frac{4.8}{203.0}$

$\frac{5.4}{210.0}$ $\frac{6.6}{210.7}$

1658

H 735+50 $\frac{7.2}{42.0}$ $\frac{6.0}{55.0}$ $\frac{6.3}{65.0}$ $\frac{7.6}{70.0}$ $\frac{6.5}{100.0}$ $\frac{4.5}{104.0}$ $\frac{4.0}{111.0}$ $\frac{4.4}{117.0}$ $\frac{8.8}{128.0}$ $\frac{14.3}{140.0}$ $\frac{14.1}{144.0}$ $\frac{7.2}{167.0}$ $\frac{5.0}{174.0}$ $\frac{3.5}{184.0}$ $\frac{3.2}{191.0}$

$\frac{6.0}{208.0}$ $\frac{6.5}{212.8}$

736 $\frac{6.9}{46.0}$ $\frac{5.4}{51.0}$ $\frac{5.2}{62.0}$ $\frac{7.2}{69.0}$ $\frac{7.5}{94.0}$ $\frac{6.2}{100.0}$ $\frac{4.0}{105.0}$ $\frac{4.0}{117.0}$ $\frac{8.3}{127.0}$ $\frac{14.4}{144.0}$ $\frac{12.8}{147.0}$ $\frac{7.3}{166.0}$ $\frac{5.8}{174.0}$ $\frac{3.6}{183.0}$ $\frac{3.3}{191.0}$

$\frac{4.9}{214.9}$

+50 $\frac{5.0}{50.0}$ $\frac{5.2}{61.0}$ $\frac{7.3}{69.0}$ $\frac{10.9}{100.0}$ $\frac{11.2}{103.4}$ $\frac{11.0}{115.0}$ $\frac{9.1}{129.0}$ $\frac{14.6}{140.0}$ $\frac{14.8}{148.0}$ $\frac{7.8}{166.0}$ $\frac{4.0}{183.0}$ $\frac{3.1}{191.6}$ $\frac{3.8}{200.0}$ $\frac{5.1}{215.7}$

737 $\frac{5.1}{49.0}$ $\frac{4.3}{61.0}$ $\frac{7.1}{90.0}$ $\frac{7.0}{98.0}$ $\frac{6.3}{100.0}$ $\frac{3.9}{105.0}$ $\frac{3.8}{117.0}$ $\frac{8.0}{129.0}$ $\frac{12.6}{140.0}$ $\frac{14.5}{144.0}$ $\frac{14.5}{148.0}$ $\frac{11.0}{158.0}$ $\frac{5.9}{177.0}$ $\frac{3.7}{183.0}$ $\frac{3.7}{200.0}$ $\frac{5.4}{215.0}$ $\frac{6.3}{216.5}$

H 737/450 $\frac{5.1}{48.0}$ $\frac{4.9}{57.0}$ $\frac{7.2}{71.0}$ $\frac{6.8}{98.0}$ $\frac{6.2}{102.0}$ $\frac{4.0}{106.0}$ $\frac{3.7}{116.0}$ $\frac{9.2}{130.0}$ $\frac{14.5}{145.0}$ $\frac{11.3}{157.0}$ $\frac{6.1}{178.0}$ $\frac{3.6}{183.0}$ $\frac{3.7}{200.0}$ $\frac{5.3}{217.0}$ $\frac{7.1}{218.4}$

738 $\frac{5.6}{44.5}$ $\frac{4.1}{51.0}$ $\frac{4.2}{62.0}$ $\frac{7.2}{72.0}$ $\frac{7.0}{98.0}$ $\frac{6.3}{103.0}$ $\frac{4.1}{107.0}$ $\frac{3.8}{119.0}$ $\frac{14.6}{145.0}$ $\frac{12.4}{151.0}$ $\frac{11.3}{159.0}$ $\frac{5.8}{176.0}$ $\frac{3.8}{186.0}$ $\frac{3.6}{200.0}$ $\frac{5.4}{208.0}$ $\frac{7.2}{220.3}$

450 $\frac{4.0}{62.0}$ $\frac{6.8}{73.0}$ $\frac{7.3}{75.0}$ $\frac{6.0}{100.0}$ $\frac{5.9}{103.0}$ $\frac{4.4}{107.0}$ $\frac{4.1}{120.0}$ $\frac{8.7}{132.0}$ $\frac{11.3}{139.0}$ $\frac{14.4}{147.0}$ $\frac{14.2}{152.0}$ $\frac{11.1}{162.0}$ $\frac{6.0}{178.0}$ $\frac{3.7}{190.0}$ $\frac{3.2}{200.0}$ $\frac{3.2}{206.0}$

$\frac{5.0}{210.0}$ $\frac{6.5}{215.0}$ $\frac{5.8}{220.0}$ $\frac{7.0}{222.2}$

739 $\frac{4.0}{55.0}$ $\frac{4.9}{61.0}$ $\frac{7.9}{75.0}$ $\frac{7.8}{94.0}$ $\frac{5.4}{108.0}$ $\frac{4.4}{105.0}$ $\frac{4.1}{120.0}$ $\frac{8.4}{131.0}$ $\frac{11.3}{141.0}$ $\frac{14.0}{148.0}$ $\frac{14.2}{152.0}$ $\frac{11.2}{160.0}$ $\frac{6.6}{172.0}$ $\frac{3.5}{187.0}$ $\frac{3.0}{200.0}$ $\frac{3.6}{216.0}$

$\frac{4.2}{220.0}$ $\frac{7.1}{224'}$

1660

4739+50 $\frac{4.1}{57.0}$ $\frac{4.1}{62.5}$ $\frac{10.5}{77.0}$ $\frac{10.2}{90.0}$ $\frac{5.8}{100.0}$ $\frac{4.5}{102.5}$ $\frac{3.9}{119.0}$ $\frac{8.5}{132.0}$ $\frac{14.3}{150.0}$ $\frac{13.5}{155.0}$ $\frac{8.3}{170.0}$ $\frac{5.1}{184.0}$ $\frac{3.4}{200.0}$ $\frac{4.8}{224.5}$ $\frac{6.7}{226.0}$

+548Δ $\frac{4.5}{50.0}$ $\frac{4.5}{64.0}$ $\frac{10.8}{77.0}$ $\frac{10.8}{91.0}$ $\frac{6.3}{100.0}$ $\frac{4.9}{103.0}$ $\frac{3.9}{120.0}$ $\frac{8.4}{132.5}$ $\frac{14.3}{151.0}$ $\frac{14.2}{157.5}$ $\frac{12.3}{163.0}$ $\frac{5.2}{184.0}$ $\frac{3.1}{200.0}$ $\frac{4.0}{227.0}$ $\frac{5.4}{227.9}$

+70 $\frac{5.9}{63.0}$ $\frac{12.3}{74.0}$ $\frac{12.8}{87.0}$ $\frac{5.0}{102.0}$ $\frac{4.7}{124.0}$ $\frac{9.4}{141.0}$ $\frac{13.9}{151.0}$ $\frac{13.9}{154.5}$ $\frac{11.4}{189.0}$ $\frac{3.0}{228.4}$

443 $\frac{12.8}{60.0}$ $\frac{14.4}{73.0}$ $\frac{15.1}{87.0}$ $\frac{15.3}{100.0}$ $\frac{15.0}{122.0}$ $\frac{14.2}{141.5}$ $\frac{13.7}{150.0}$ $\frac{14.0}{190.0}$ $\frac{6.8}{219.0}$

1661

Original Cross Sections of Borrow Pit

H 740+02.8 $\frac{12.8}{35.0}$ $\frac{14.2}{63.0}$ $\frac{14.6}{74.0}$ $\frac{14.8}{87.0}$ $\frac{13.4}{100.0}$ $\frac{14.8}{121.0}$ $\frac{13.9}{141.5}$ $\frac{13.5}{151.0}$ $\frac{14.2}{187.0}$ $\frac{11.4}{223.9}$

H 921 $\frac{8.1}{114.0}$ $\frac{6.8}{128.0}$ $\frac{4.9}{152.0}$ $\frac{3.2}{170.0}$ $\frac{3.3}{185.0}$ $\frac{4.2}{200.0}$

150 $\frac{9.9}{75.0}$ $\frac{6.2}{92.0}$ $\frac{5.2}{115.0}$ $\frac{7.3}{126.0}$ $\frac{4.9}{136.0}$ $\frac{5.1}{150.0}$ $\frac{4.1}{162.0}$ $\frac{3.9}{180.0}$

$\frac{5.0}{236.0}$ $\frac{7.2}{255.0}$ $\frac{7.1}{300.0}$

H 742 1

$\frac{10.2}{65.0}$ $\frac{5.9}{64.0}$ $\frac{4.5}{100.0}$ $\frac{5.0}{135.0}$ $\frac{7.3}{148.0}$ $\frac{7.2}{174.0}$ $\frac{7.7}{180.0}$ $\frac{7.2}{185.0}$

$\frac{5.7}{200.0}$ $\frac{6.4}{278.0}$ $\frac{6.8}{300.0}$

+50

$\frac{6.5}{64.0}$ $\frac{4.4}{100.0}$ $\frac{3.6}{135.0}$ $\frac{4.4}{143.0}$ $\frac{5.7}{148.0}$ $\frac{5.9}{167.0}$ $\frac{7.2}{175.0}$ $\frac{7.3}{200.0}$

$\frac{7.7}{254.0}$ $\frac{7.5}{300.0}$

743

$\frac{4.1}{62.0}$ $\frac{4.2}{100.0}$ $\frac{4.6}{135.0}$ $\frac{4.9}{157.0}$ $\frac{5.8}{174.0}$ $\frac{7.6}{186.0}$ $\frac{7.6}{200.0}$

$\frac{7.9}{250.0}$ $\frac{7.7}{300.0}$

+50

$\frac{9.3}{69.0}$ $\frac{4.1}{100.0}$ $\frac{4.9}{135.0}$ $\frac{5.7}{146.0}$ $\frac{7.6}{169.0}$ $\frac{8.0}{185.0}$ $\frac{8.2}{200.0}$ $\frac{7.6}{250.0}$

$\frac{7.7}{300.0}$

1663

H 7.4

$\frac{4.0}{110.0}$ $\frac{4.5}{130.0}$ $\frac{5.6}{116.0}$ $\frac{7.2}{135.0}$ $\frac{7.7}{154.0}$ $\frac{8.1}{185.0}$ $\frac{7.8}{200.0}$ $\frac{7.8}{255.0}$

$\frac{7.7}{300.0}$

7.50

$\frac{6.2}{67.0}$ $\frac{6.4}{100.0}$ $\frac{7.2}{127.0}$ $\frac{7.3}{125.0}$ $\frac{7.5}{147.0}$ $\frac{7.0}{163.0}$ $\frac{7.7}{170.0}$ $\frac{7.7}{185.0}$

$\frac{7.7}{200.0}$ $\frac{7.9}{252.0}$ $\frac{7.7}{300.0}$

9.5

$\frac{5.0}{68.0}$ $\frac{5.3}{100.0}$ $\frac{5.7}{125.0}$ $\frac{5.9}{148.0}$ $\frac{7.0}{154.0}$ $\frac{6.8}{170.0}$ $\frac{7.1}{185.0}$ $\frac{7.6}{200.0}$

$\frac{7.6}{253.0}$ $\frac{7.7}{300.0}$

7.60

7 $\frac{5.9}{253}$

$\frac{5.0}{68.0}$ $\frac{5.0}{100.0}$ $\frac{6.4}{135.0}$ $\frac{5.7}{164.0}$ $\frac{6.9}{170.0}$ $\frac{7.0}{185.0}$ $\frac{7.1}{200}$ $\frac{7.6}{210.0}$ $\frac{7.8}{245.0}$

$\frac{7.4}{300.0}$

1664

-Original-
Cross Section of Cross Levee at H 940+03.8

H 940+03.8 △ 19.00

Level

These X Secs. Superseded by those on Page 50.

		Lt				C	Rt			
0+0.0										
0+17.6					0.0 4.0	0.0	0.0 4.0			
0+30		R.R. Grade -6.4 10.0		-4.6 6.5	-4.7 4.0	-6.2	-8.2 4.0	R.R. Grade		
0+45	R.R. Grade -12.6 39.5	-11.8 35.0	-6.1 13.0	-4.7 8.0	-4.5 4.0	-5.9	-8.8 4.0	-9.9 5.0	-8.9 14.0	-9.8 18.4
0+50		-12.0 45.0	-12.3 34.0	-5.3 11.0	-4.6 4.0	-6.0	-8.3 4.0	-9.4 17.0	-12.7 21.8	
0+63		-11.8 38.4	-11.0 23.0	-4.6 10.0	-4.4 4.0	-4.9	-6.8 4.0	-8.5 11.5	-12.8 23.2	
0+73				-4.8 10.4	-4.2 4.0	-4.2	-4.3 4.0	-5.3 12.0		
0+88				-4.8 12.	-4.0 4.0	-4.0	-3.7 4.0	-4.9 11.5		

1665

				Lt			C		Rt		
1+00			-10.1/34.3	-10.6/28.0	-7.2/17.0	-4.9/4.0	-3.6	-3.6/4.0	-8.7/13.0	-11.7/21.6	
1+27			Same			-4.7/4.0	-3.6	-4.1/4.0	-10.5/15.5	-11.7/21.0	
1+50			-13.6/44.7	-12.9/31.0	-10.2/20.0	-4.7/4.0	-5.0	-4.3/4.0	-4.8/5.5	-6.6/13.9	
1+80.3△	-15.0/49.0	-15.9/46.0	-16.8/37.0	-12.1/27.0	-9.9/14.0	-5.0/4.0	-4.5	-5.1/4.0	-7.7/10.0	-9.9/14.0	-15.0/28.5
2+00	-15.3/49.9	-15.7	-15.6/37.6	-11.6/25.5	-8.1/16.0	-5.4/4.0	-4.6	-4.8/4.0	-8.0/11.5	-11.0/30.5	
2+26			-15.3/45.0	-15.5/39.0	-11.2/22.0	-5.6/4.0	-4.6	-4.7/4.0	-9.2/16.0	-11.1/30.7	

Cross Sections for August 1909 Estimate

September 1st 09

Rt.

#741+50	original cross section					
742	$\frac{9.9}{47.0}$	$\frac{5.6}{65.0}$	$\frac{4.4}{94.0}$	$\frac{3.3}{112.0}$	$\frac{4.9}{122.0}$	$\frac{5.0}{135.0}$
+50	$\frac{6.5}{65.0}$	$\frac{2.7}{80.0}$	$\frac{2.3}{103.0}$	$\frac{3.1}{132.0}$	$\frac{3.3}{134.0}$	
743	$\frac{4.1}{62.0}$	$\frac{3.4}{65.0}$	$\frac{3.3}{100.0}$	$\frac{2.8}{131.0}$	$\frac{4.5}{134.0}$	
+50	$\frac{3.8}{72.0}$	$\frac{2.8}{75.0}$	$\frac{2.9}{105.0}$	$\frac{3.4}{132.0}$	$\frac{4.9}{134.0}$	

1667

Cross Sections for August 1909

744

H 744	$\frac{4.0}{71.0}$	$\frac{3.2}{76.0}$	$\frac{3.3}{94.0}$	$\frac{4.0}{131.0}$	$\frac{7.9}{134.5}$
+50	$\frac{5.1}{69.0}$	$\frac{3.5}{74.0}$	$\frac{3.2}{98.0}$	$\frac{4.8}{131.0}$	$\frac{7.1}{134.0}$
745	$\frac{5.0}{68.0}$	$\frac{2.9}{70.0}$	$\frac{3.2}{98.0}$	$\frac{3.4}{131.0}$	$\frac{5.7}{134.5}$
+50	$\frac{5.0}{69.0}$	$\frac{3.2}{74.0}$	$\frac{3.3}{102.0}$	$\frac{5.3}{123.0}$	$\frac{5.6}{134.0}$
746	$\frac{5.2}{69.0}$	$\frac{3.3}{70.0}$	$\frac{3.4}{131.0}$	$\frac{5.7}{134.5}$	

Cross-Sections for August 1909

H 746+50	$\frac{5.4}{69.0}$	$\frac{3.5}{74.0}$	$\frac{3.8}{100.0}$	$\frac{3.9}{131.0}$	$\frac{6.0}{134.5}$
747	$\frac{7.1}{63.0}$	$\frac{5.3}{74.0}$	$\frac{5.1}{98.0}$	$\frac{5.4}{130.0}$	$\frac{7.0}{133.5}$
+50	$\frac{7.3}{71.0}$	$\frac{6.1}{75.0}$	$\frac{5.8}{98.0}$	$\frac{6.3}{130.0}$	$\frac{7.9}{133.0}$
748	$\frac{7.2}{69.0}$	$\frac{6.0}{74.0}$	$\frac{6.4}{100.0}$	$\frac{6.2}{130.0}$	$\frac{7.8}{134.0}$
+30	Original Cross Section				

P.E.D.

Cross Sections for September 1909

H.D. Millard contractor

September 30th 09

H 748+30

Original Cross Section

748 $\frac{7.8}{69.0}$ $\frac{6.1}{72.0}$ $\frac{5.8}{78.0}$ $\frac{5.0}{100.0}$ $\frac{4.6}{113.0}$ $\frac{5.8}{128.0}$ $\frac{7.8}{137.0}$

747 $\frac{2.1}{63.0}$ $\frac{2.6}{73.0}$ $\frac{1.8}{86.0}$ $\frac{1.0}{100.0}$ $\frac{1.6}{107.0}$ $\frac{1.4}{121.0}$ $\frac{7.0}{133.5}$

746 $\frac{5.2}{69.0}$ $\frac{1.1}{85.0}$ $\frac{-0.5}{103.0}$ $\frac{-1.0}{115.0}$ — $\frac{0.2}{126.0}$ $\frac{2.2}{133.0}$ $\frac{5.2}{160.0}$ $\frac{6.1}{184.0}$ $\frac{7.0}{185.0}$

745 $\frac{5.2}{68.0}$ $\frac{1.8}{77.0}$ $\frac{1.0}{81.0}$ $\frac{1.4}{110.0}$ $\frac{1.9}{126.0}$ $\frac{3.2}{128.0}$ $\frac{4.8}{137.0}$ $\frac{6.4}{183.0}$ $\frac{7.1}{185.0}$

Cross Sections for September 1909

H. 744

743

742

741 +60

741

744

$\frac{4.1}{71.0}$ $\frac{1.8}{76.5}$ $\frac{3.3}{84.0}$ $\frac{2.1}{100.0}$ $\frac{2.6}{120.0}$ $\frac{3.6}{135.0}$ $\frac{5.8}{159.0}$ $\frac{6.3}{180.0}$ $\frac{8.1}{184.0}$

$\frac{4.3}{53.0}$ $\frac{4.5}{66.0}$ $\frac{4.2}{78.0}$ $\frac{4.9}{100.0}$ $\frac{3.1}{130.0}$ $\frac{4.3}{175.0}$ $\frac{6.3}{180.0}$ $\frac{7.5}{184.5}$

$\frac{8.1}{55.0}$ $\frac{4.8}{69.0}$ $\frac{4.0}{84.0}$ $\frac{3.0}{100.0}$ $\frac{5.3}{125.0}$ $\frac{4.5}{160.0}$ $\frac{6.4}{192.0}$

$\frac{9.9}{75}$ $\frac{8.2}{81.0}$ $\frac{3.3}{84.0}$ $\frac{2.1}{100.0}$ $\frac{3.5}{120.0}$ $\frac{4.9}{150.0}$ $\frac{5.1}{160.0}$

Original Cross Section

Cross Sections for September 1909.

Rt

Original Cross Section

H 739						
738	$\frac{3.8}{119.0}$	$\frac{11.6}{136.0}$	$\frac{12.0}{144.0}$	$\frac{12.0}{147.0}$	$\frac{12.3}{153.0}$	$\frac{11.3}{157.0}$
737			$\frac{7.0}{129.0}$	$\frac{12.4}{139.0}$	$\frac{12.4}{150.0}$	$\frac{11.0}{157.0}$
736			$\frac{8.3}{137.0}$	$\frac{11.7}{139.0}$	$\frac{13.1}{148.0}$	$\frac{7.9}{166.0}$
735		$\frac{2.6}{127.0}$	$\frac{11.7}{137.0}$	$\frac{12.8}{142.0}$	$\frac{12.5}{149.0}$	$\frac{8.3}{164.0}$

1672

Cross Sections for September 1909

Rt

H 734	$\frac{12.4}{134.0}$	$\frac{13.8}{140.0}$	$\frac{12.4}{149.0}$	$\frac{11.6}{153.0}$	
733	$\frac{11.6}{124.0}$	$\frac{13.3}{135.0}$	$\frac{13.6}{141.0}$	$\frac{12.9}{150.0}$	$\frac{11.5}{155.0}$
732	$\frac{11.5}{122.0}$	$\frac{12.4}{128.0}$	$\frac{13.5}{138.0}$	$\frac{12.8}{147.5}$	$\frac{11.8}{152.0}$
731	$\frac{11.3}{122.0}$	$\frac{12.7}{130.0}$	$\frac{12.5}{142.0}$	$\frac{11.4}{150.0}$	
730	$\frac{10.2}{120.0}$	$\frac{11.9}{128.0}$	$\frac{12.1}{135.0}$	$\frac{11.8}{143.0}$	$\frac{9.8}{156.0}$
729					

Original Cross Section J.E.D.

Cross Sections for October 1909 H. D. Millard contractor

October 30, 1909

75'

H 739+54 3/21 Original Cross Sections

H 739+50	$\frac{5.9}{119°}$	$\frac{5.5}{123°}$	$\frac{7.6}{141°}$	$\frac{7.4}{150°}$	$\frac{6.8}{167°}$	$\frac{6.1}{181°}$	$\frac{5.1}{184°}$
739		$\frac{4.1}{120°}$	$\frac{4.7}{135°}$	$\frac{4.5}{145°}$	$\frac{4.6}{167°}$	$\frac{4.0}{181°}$	$\frac{3.5}{185°}$
738	$\frac{3.8}{112°}$	$\frac{5.7}{107°}$	$\frac{5.7}{145°}$	$\frac{5.1}{165°}$	$\frac{4.1}{170°}$	$\frac{3.8}{186°}$	
737		$\frac{3.9}{117°}$	$\frac{5.1}{129°}$	$\frac{6.3}{142°}$	$\frac{5.8}{164°}$	$\frac{5.0}{176°}$	$\frac{3.7}{188°}$

1674

Cross Sections for October 1909 H. D. Millard Contractor

Rt

A H 736	$\frac{4.0}{112.0}$	$\frac{5.6}{122.0}$	$\frac{5.8}{[illegible]}$	$\frac{7.3}{150.0}$	$\frac{6.6}{153.0}$	$\frac{5.8}{174.0}$	
735	$\frac{2.6}{116.0}$	$\frac{5.8}{118.0}$	$\frac{5.6}{122.0}$	$\frac{5.7}{147.0}$	$\frac{6}{160.0}$	$\frac{5.6}{171.0}$	$\frac{3.6}{180.0}$
734	$\frac{5.7}{114.0}$	$\frac{6.8}{117.0}$	$\frac{6.8}{128.0}$	$\frac{7.8}{141.0}$	$\frac{5.8}{162.0}$	$\frac{5.8}{177.0}$	
733	$\frac{6.9}{114.0}$	$\frac{7.3}{117.0}$	$\frac{8.1}{126.0}$	$\frac{8.9}{142.0}$	$\frac{6.9}{160.5}$	$\frac{6.1}{172.5}$	
732	$\frac{6.9}{112.0}$	$\frac{7.6}{125.0}$	$\frac{7.7}{124.0}$	$\frac{8.3}{142.0}$	$\frac{7.5}{158.0}$	$\frac{6.5}{169.0}$	

1675

Cross Sections for October 1909 H. D. Millard Contractor

781

H. H. 781	$\frac{6.7}{110.0}$	$\frac{7.0}{118.0}$	$\frac{7.5}{121.0}$	$\frac{8.2}{142.0}$	$\frac{8.0}{154.0}$	$\frac{6.8}{166.0}$	$\frac{4.6}{174.0}$
780	$\frac{6.5}{111.0}$	$\frac{7.3}{124.0}$	$\frac{8.8}{133.0}$	$\frac{7.7}{157.0}$	$\frac{6.9}{164.0}$		
779	$\frac{6.6}{116.0}$	$\frac{8.0}{123.0}$	$\frac{9.0}{129.0}$	$\frac{7.0}{143.0}$	$\frac{8.9}{155.0}$	$\frac{9.5}{168.0}$	
778	$\frac{6.7}{106.0}$	$\frac{7.3}{116.0}$	$\frac{7.8}{125.0}$	$\frac{8.8}{140.0}$	$\frac{9.0}{152.0}$	$\frac{7.9}{155.0}$	
777	$\frac{5.9}{103.0}$	$\frac{6.9}{111.0}$	$\frac{7.7}{125.0}$	$\frac{8.9}{142.0}$	$\frac{8.6}{149.0}$	$\frac{7.1}{169.0}$	

Cross Sections for October 1909 H. D. Millard Contractor

Rt

H 726	$\frac{5.0}{100.0}$	$\frac{6.7}{110.0}$	$\frac{7.7}{122.0}$	$\frac{8.2}{133.0}$	$\frac{8.5}{141.0}$	$\frac{5.5}{157.0}$
725	$\frac{4.1}{97.0}$	$\frac{5.7}{115.0}$	$\frac{7.9}{124.0}$	$\frac{8.1}{130.0}$	$\frac{7.2}{138.0}$	$\frac{6.9}{147.0}$
724	$\frac{4.7}{97.0}$	$\frac{6.2}{109.0}$	$\frac{7.7}{122.0}$	$\frac{7.7}{140.0}$	$\frac{6.6}{146.0}$	
723	$\frac{4.0}{93.0}$	$\frac{5.6}{108.0}$	$\frac{6.8}{114.0}$	$\frac{6.9}{127.0}$	$\frac{7.4}{141.0}$	$\frac{5.9}{146.0}$
722	$\frac{3.9}{85.0}$	$\frac{5.3}{113.0}$	$\frac{7.7}{118.0}$	$\frac{8.0}{131.0}$	$\frac{7.5}{140.0}$	$\frac{5.9}{145.0}$

1677

Cross Sections for October 1909 H. D. Millard Contractor

Ht

H 721	$\frac{4^9}{93^0}$	$\frac{5^6}{100^0}$	$\frac{6^4}{118^0}$	$\frac{7^1}{127^0}$	$\frac{6^8}{137^0}$	$\frac{6^1}{139^0}$
720	$\frac{7^1}{87^0}$	$\frac{7^0}{103^0}$	$\frac{7^2}{113^0}$	$\frac{7^9}{132^0}$	$\frac{5^8}{137^0}$	
719+65	$\frac{6^2}{91^0}$	$\frac{7^4}{100^0}$	$\frac{8^2}{111^0}$	$\frac{8^6}{132^0}$	$\frac{6^3}{141^0}$	
719+84½ Δ	Original Cross Section					

P.E.L.

1678

33

Cross Sections for November 1909 H. D. Millard contractor

Rt

H 740 Original Cross Section

739+50 $\frac{3.9}{119.0}$ $\frac{7.7}{142.0}$ $\frac{7.3}{158.0}$ $\frac{6.3}{178.0}$ $\frac{3.4}{200.0}$

739 $\frac{4.1}{119.0}$ $\frac{4.8}{138.0}$ $\frac{4.8}{164.0}$ $\frac{3.5}{189.0}$

738 $\frac{4.2}{61.0}$ $\frac{5.9}{72.0}$ $\frac{6.6}{83.0}$ $\frac{4.8}{100.0}$ $\frac{3.2}{111.0}$ $\frac{4.6}{127.0}$ $\frac{4.7}{151.0}$ $\frac{4.0}{172.0}$ $\frac{3.8}{186.0}$

737 $\frac{4.2}{61.0}$ $\frac{6.1}{89.0}$ $\frac{6.0}{87.0}$ $\frac{6.2}{99.0}$ $\frac{3.6}{118.0}$ $\frac{5.8}{134.0}$ $\frac{5.1}{159.0}$ $\frac{3.9}{174.0}$

Cross Section for November 1909 H. D. Millard – contractor

Rt

H 236		5.3/63.0	6.9/78.0	6.4/90.0	7.8/100.0	3.3/116.0	5.1/126.0	5.9/162.0	5.5/174.0
235	6.5/31.0	6.8/66.0	6.4/78.0	5.4/100.0	3.7/112.0	5.1/123.0	5.8/148.0	7.4/169.0	5.6/190.0
234		5.8/49.0	6.4/61.0	8.0/70.0	7.3/100.0	5.2/117.0	6.7/131.0	6.6/163.0	5.8/177.0
233	8.8/47.0	7.8/55.0	2.8/67.0	9.0/92.5	6.2/110.0	6.8/125.0	6.9/155.0	5.0/165.0	6.1/172.0
232	7.2/48.0	8.7/61.0	8.1/68.0	8.5/92.0	5.8/106.0	7.4/119.0	6.6/127.0	7.4/144.0	6.5/169.0

1680

Cross Sections for November 1909 H. J. Millard contractor

84

H 731 $\frac{7.9}{47.0}$ $\frac{9.0}{62.0}$ $\frac{8.3}{74.0}$ $\frac{7.8}{86.0}$ $\frac{6.5}{100.0}$ $\frac{5.5}{107.0}$ $\frac{6.6}{121.0}$ $\frac{6.7}{145.0}$ $\frac{7.5}{168.0}$

H 730 [illegible] $\frac{8.4}{62.0}$ $\frac{7.3}{73.0}$ $\frac{8.2}{99.0}$ $\frac{6.1}{125.0}$ $\frac{6.1}{142.0}$ $\frac{6.0}{153.0}$ $\frac{6.2}{155}$ ~~$\frac{7.0}{167}$~~ $\frac{6.3}{164}$

729 $\frac{7.8}{39.0}$ $\frac{8.2}{61.0}$ $\frac{6.9}{79.0}$ $\frac{6.8}{90.0}$ $\frac{6.1}{100.0}$ $\frac{6.1}{110.0}$ $\frac{7.8}{135.0}$ $\frac{7.5}{158.0}$

728 $\frac{7.8}{62.0}$ $\frac{6.1}{71.0}$ $\frac{7.0}{85.0}$ $\frac{5.9}{100.0}$ $\frac{6.2}{110.0}$ $\frac{7.1}{138.0}$ $\frac{7.4}{155.0}$

727 $\frac{8.1}{64.0}$ $\frac{6.0}{78.0}$ $\frac{6.4}{90.0}$ $\frac{5.0}{100.0}$ $\frac{6.5}{121.0}$ $\frac{6.4}{141.0}$ $\frac{7.1}{154.0}$

1681

36

Cross Section for November 1909   H. D. Millard contractor

H 726 $\frac{2.9}{55.5}$ $\frac{5.0}{65.0}$ $\frac{5.5}{71.0}$ $\frac{6.3}{89.0}$ $\frac{4.6}{100.0}$ $\frac{5.9}{110.0}$ $\frac{5.2}{125.0}$ $\frac{6.5}{146.0}$ $\frac{5.5}{157.0}$

725    $\frac{7.9}{57.0}$ $\frac{3.1}{63.0}$ $\frac{2.6}{74.0}$ $\frac{2.5}{87.0}$ $\frac{2.9}{100.0}$ $\frac{3.1}{123.0}$ $\frac{2.8}{130.0}$ $\frac{2.2}{166.0}$ $\frac{4.1}{173.0}$

724    $\frac{7.8}{55.0}$ $\frac{2.3}{64.0}$ $\frac{2.0}{74.0}$ $\frac{2.4}{86.0}$ $\frac{2.2}{124.0}$ [illegible] $\frac{4.6}{166.0}$

723    $\frac{7.9}{57.0}$ $\frac{2.4}{68.0}$ $\frac{4.1}{82.0}$ $\frac{1.8}{91.0}$ $\frac{2.2}{100.0}$ $\frac{2.8}{120.0}$ $\frac{2.8}{148.0}$ $\frac{2.4}{157.0}$ $\frac{4.6}{162.0}$

722    $\frac{7.6}{56.0}$ $\frac{3.9}{65.0}$ $\frac{3.3}{83.0}$ $\frac{1.2}{100.0}$ $\frac{1.4}{114.0}$ $\frac{2.5}{137.0}$ $\frac{2.9}{155.0}$ $\frac{4.6}{158.0}$

1682

Cross Sections for November 1909 H. D. Millard contractor

Rt.

H721 $\frac{7.9}{57.0}$ $\frac{3.1}{[illegible]}$ $\frac{2.1}{83.0}$ $\frac{2.2}{88.0}$ $\frac{2.9}{100.0}$ $\frac{1.4}{119.0}$ $\frac{2.2}{128.0}$ $\frac{3.3}{144.0}$ $\frac{4.9}{152.0}$

720 $\frac{9.0}{55.0}$ $\frac{2.2}{66.0}$ $\frac{2.4}{83.0}$ $\frac{2.5}{100.0}$ $\frac{2.9}{122.0}$ $\frac{3.8}{141.0}$ $\frac{7.2}{148.0}$

719+65 Same as for October 1909 Estimate

Cross Sections for November 1903 H. D. Millard contractor

Rt

H 241 Same as for October 1903

242 $\frac{5.8}{156.0}$ $\frac{3.2}{157.0}$ $\frac{4.6}{161.0}$ $\frac{2.5}{176.0}$ $\frac{2.7}{182.0}$ $\frac{4.8}{211.0}$ $\frac{4.1}{240.0}$ $\frac{6.2}{266.0}$ $\frac{7.5}{277.0}$

243 $\frac{5.1}{150.0}$ $\frac{3.2}{160.0}$ $\frac{4.8}{178.0}$ $\frac{2.8}{200.0}$ $\frac{3.2}{246.0}$ $\frac{3.5}{260.0}$ $\frac{7.6}{298.0}$

244 $\frac{5.2}{157.0}$ $\frac{4.1}{161.0}$ $\frac{2.5}{171.0}$ $\frac{2.8}{200.0}$ $\frac{4.2}{223.0}$ $\frac{2.6}{254.0}$ $\frac{3.7}{282.0}$ $\frac{7.7}{290.0}$

245 $\frac{3.7}{158.0}$ $\frac{4.1}{164.0}$ $\frac{1.9}{180.0}$ $\frac{3.7}{191.0}$ $\frac{2.9}{200.0}$ $\frac{3.6}{218.0}$ $\frac{2.1}{266.0}$ $\frac{7.7}{277.0}$

1684

Cross Sections for November 1909 H. D. Millard contractor

Rt

H746 $\frac{3.3}{125.0}$ $\frac{3.7}{133.0}$ $\frac{2.0}{144.0}$ $\frac{3.1}{165.0}$ $\frac{2.1}{200.0}$ $\frac{1.9}{236.0}$ $\frac{2.2}{249.0}$

747 $\frac{1.4}{170}$ $\frac{1.2}{185.0}$ $\frac{2.4}{180.0}$ $\frac{2.3}{178.0}$ $\frac{1.8}{210.0}$ $\frac{7.0}{212.0}$

748 $\frac{5.0}{160.0}$ $\frac{4.0}{25.0}$ $\frac{4.6}{167.0}$ $\frac{3.6}{188.0}$ $\frac{3.4}{210.0}$ $\frac{7.8}{214.0}$

750 Original Cross Section

Cross Sections for December 1909 H. B. Hillard contractor

Sta Rt

H 748 Same as for November 1909

747 $\frac{1.4}{117.0}$ $\frac{1.5}{135.0}$ $\frac{1.0}{157.0}$ $\frac{1.1}{178.0}$ $\frac{1.6}{206.0}$ $\frac{7.0}{212.0}$

746 $\frac{3.7}{122.0}$ $\frac{1.5}{135.0}$ $\frac{0.5}{144.0}$ $\frac{1.3}{165.0}$ $\frac{0.8}{200.0}$ $\frac{2.0}{228.0}$ $\frac{2.2}{249.0}$

745 $\frac{3.9}{135.0}$ $\frac{2.3}{140.0}$ $\frac{1.6}{160.0}$ $\frac{1.4}{175.0}$ $\frac{1.6}{200.0}$ $\frac{2.1}{212.0}$ $\frac{1.6}{246.0}$ $\frac{7.7}{277.0}$

744 $\frac{5.0}{154.0}$ $\frac{2.2}{160.0}$ $\frac{3.0}{170.0}$ $\frac{2.1}{200.0}$ $\frac{2.2}{250.0}$ $\frac{1.6}{264.0}$ $\frac{1.3}{282.0}$ $\frac{7.7}{292.0}$

Cross Section for December 1909 H. D. Millards

Sta TH 16.2

H 748 3.1/135.0 2.1/150.0 1.9/160.0 1.8/175.0 1.7/200.0 1.6/210.0 2.8/255.0 7.6/298.0

H 742 Same as for November 1909

H 740 " " " " "

7-9450 6.9/91.0 5.5/95.0 5.4/95.0 5.8/100.0 4.8/105.0 4.0/110.0 5.7/135.0 5.4/160.0 6.0/170.0 5.4/200.0

729 7.6/70.0 4.2/76.0 4.4/96.0 5.0/105.0 4.4/120.0 4.2/140.0 2.9/155.0 3.9/165.0 4.1/185.0 3.5/189.0

Cross Sections for December 1909 H. D. Milbird Contractor

Sta.	
H 738	$\frac{4.2}{62.0}$ $\frac{5.1}{70.0}$ $\frac{2.3}{77.0}$ $\frac{2.3}{90.0}$ $\frac{3.0}{96.0}$ $\frac{4.6}{100.0}$ $\frac{4.8}{[illegible]}$ $\frac{2.5}{126.0}$ $\frac{4.2}{145.0}$ $\frac{2.7}{160.0}$ $\frac{4.6}{161.0}$ $\frac{4.2}{165}$ $\frac{3.4}{173.0}$ $\frac{3.8}{186.0}$
737	$\frac{4.9}{61.0}$ $\frac{6.0}{69.0}$ $\frac{4.8}{79.0}$ $\frac{3.2}{76.0}$ $\frac{4.8}{100.0}$ $\frac{4.8}{105.0}$ $\frac{3.3}{112.0}$ $\frac{4.2}{130.0}$ $\frac{5.2}{141.0}$ $\frac{3.6}{152.0}$ $\frac{4.7}{163.0}$ $\frac{4.8}{174.0}$ $\frac{5.2}{181.0}$ $\frac{3.7}{187.0}$
736	$\frac{5.2}{62.0}$ $\frac{6.0}{73.0}$ $\frac{3.5}{80.0}$ $\frac{2.6}{76.0}$ $\frac{3.3}{100.0}$ $\frac{4.2}{103.0}$ $\frac{3.4}{113.0}$ $\frac{4.6}{152.0}$ $\frac{4.6}{160.0}$ $\frac{3.3}{[illegible]}$ $\frac{5.0}{176.0}$ $\frac{4.2}{182.0}$ $\frac{3.6}{183.0}$
735 T.P. 6.54	$\frac{6.5}{56.0}$ $\frac{6.2}{62.0}$ $\frac{5.3}{65.0}$ $\frac{3.7}{77.0}$ $\frac{3.1}{72.0}$ $\frac{3.5}{102.0}$ $\frac{3.6}{107.0}$ $\frac{5.1}{115.0}$ $\frac{4.5}{120.0}$ $\frac{3.9}{136.0}$ $\frac{4.3}{156.0}$ $\frac{4.5}{177.0}$ $\frac{3.6}{183.0}$
734	$\frac{6.4}{61.0}$ $\frac{5.0}{68.0}$ $\frac{4.6}{72.0}$ $\frac{5.2}{90.0}$ $\frac{5.6}{100.0}$ $\frac{5.0}{102.0}$ $\frac{5.1}{121.0}$ $\frac{4.8}{138.0}$ $\frac{5.6}{163.0}$ $\frac{5.5}{175.0}$

Cross Section for December 1909 H. D. Millard contractor

Sta.

Ft

H 733 7.8/55.0 7.2/61.5 5.8/65.0 5.2/75.0 5.[illegible]/9[illegible] 6.7/100.0 5.6/107.0 5.9/120.0 5.7/132.0 6.2/155.0 4.8/165.0 4.9/174.0 4.7/179.0

732 7.2/48.0 7.7/57.0 6.2/65.0 5.3/81.0 5.5/92.0 6.2/100.0 5.7/111.0 6.2/120.0 6.1/137.0 6.2/153.0 5.1/164.0 4.9/176.0

731 7.9/47.0 8.5/57.0 6.4/64.0 6.0/75.0 6.3/87.0 6.0/92.0 6.1/100.0 5.6/109.0 6.4/130.0 6.3/140.0 6.7/165.0 4.6/174.0

730 8.7/49.0 8.[illegible]/5[illegible] 6.4/62.0 5.5/75.0 5.2/84.0 6.2/98.0 5.2/108.0 6.7/125.0 6.5/140.0 6.6/157.0 6.3/164.0

729 8.1/68.0 6.0/76.0 6.4/90.0 5.5/100.0 6.1/115.0 7.0/130.0 7.1/145.0 6.9/161.0

1689

Cross Sections for December 1909. H.D. Millard contractor

8/6

Rt.

H 728 $\frac{7.2}{64.0}$ $\frac{6.4}{75.0}$ $\frac{6.6}{90.0}$ $\frac{6.2}{100.0}$ $\frac{6.1}{102.0}$ $\frac{7.1}{140.0}$ $\frac{7.4}{155.0}$

727 $\frac{8.1}{34.0}$ $\frac{6.2}{70.0}$ $\frac{6.0}{[illegible]}$ $\frac{6.5}{93.0}$ $\frac{5.2}{100.0}$ $\frac{5.5}{113.0}$ $\frac{5.2}{125.0}$ $\frac{5.8}{146.0}$ $\frac{7.0}{154.0}$

726 $\frac{8.4}{[illegible]}$ $\frac{9.0}{[illegible]}$ $\frac{5.8}{67.0}$ [illegible] $\frac{6.8}{74.0}$ $\frac{6.5}{91.0}$ $\frac{4.6}{106.0}$ $\frac{6.3}{120.0}$ $\frac{6.4}{136.0}$ $\frac{5.4}{144.0}$ $\frac{5.2}{155.0}$ $\frac{5.5}{157}$

725 Same as for November 1909

P.E.D.

Cross Sections for January 1910 H. D. Millard Contractor

TPT Feb. 3 1910

Sta

H 740 Same as for November 1909

739+50 $\frac{6.4}{125.0}$ $\frac{5.9}{140.0}$ $\frac{3.9}{117.0}$ $\frac{5.2}{135.0}$ $\frac{5.7}{155.0}$ $\frac{5.8}{183.0}$ $\frac{3.2}{200.0}$

737 $\frac{4.4}{95.0}$ $\frac{4.5}{100.0}$ $\frac{4.6}{120.0}$ $\frac{3.0}{140.0}$ $\frac{2.8}{155.0}$ $\frac{3.8}{165.0}$ $\frac{4.1}{185.0}$

736 Same as for Dec 09 $\frac{4.1}{164.0}$ $\frac{5.2}{173.0}$ $\frac{3.8}{186.0}$

737 to 735 Same as for December 1909

735 Same as for December 1909

734 $\frac{5.6}{103.0}$ $\frac{5.0}{107.0}$ $\frac{5.7}{121.0}$ $\frac{4.3}{140.0}$ $\frac{4.9}{160.0}$ $\frac{5.5}{176.0}$

733 $\frac{6.7}{100.0}$ $\frac{5.6}{117.0}$ $\frac{5.7}{120.0}$ $\frac{4.7}{144.0}$

Cross Sections for January 1910

Sta

H 783

731

H. D. Millard contractor

Rt

$\frac{62}{103.0}$ $\frac{57}{111.0}$ $\frac{58}{130.0}$ $\frac{59}{145.0}$ $\frac{53}{158.0}$ $\frac{51}{174.0}$ $\frac{49}{196.0}$

Same as for December 1909

P. E. D.

1692

Cross Sections for January 1910 H. H. Millard Contractor

North Levee opposite H740+03.8 to H741+75 Left C.

February 12, 1910

H740+03.8 B.C.T.3			$\frac{7.4}{50.0}$ R.W.	$\frac{9.6}{48.0}$	$\frac{12.4}{31.0}$	$\frac{15.0}{22.4}$
+33.8		$\frac{7.5}{62.0}$	$\frac{10.4}{55.0}$	$\frac{10.6}{50.0}$ R.W.	$\frac{10.6}{42.5}$	$\frac{10.0}{28.5}$
+63.8		$\frac{7.7}{79.0}$	$\frac{11.1}{62.0}$	$\frac{10.9}{50.0}$ R.W.	$\frac{10.2}{36.0}$	$\frac{8.8}{33.1}$
741	[illegible]	$\frac{8.2}{91.5}$	$\frac{9.4}{72.0}$	$\frac{10.0}{63.0}$	$\frac{9.4}{54.0}$	$\frac{8.4}{50.0}$ R.W.
+25	[illegible]	$\frac{7.8}{110.0}$	$\frac{9.1}{100.0}$	$\frac{7.8}{84.0}$	$\frac{8.4}{67.5}$	$\frac{8.3}{62.0}$
+50		$\frac{8.0}{136.0}$	$\frac{7.7}{129.0}$	$\frac{7.7}{100.0}$	$\frac{7.9}{84.0}$	$\frac{8.5}{72.0}$
+75		$\frac{8.1}{129.0}$	$\frac{7.6}{105.0}$	$\frac{7.4}{100.0}$	$\frac{7.5}{94.0}$	$\frac{8.1}{83.8}$

Note See letter by H.V. Moffat, December 1909 for original cross sections.

Material taken inside of R.W. dumped on grade, outside of R.W. on road approach. private contract

Note— this estimate includes a few hours Work during February 1 to 10; see detail time reports for time of teams working on S.P. work opposite these stations

X Sections for June 1910.

June Estimate

H. D. Millard Contr.

Sta.		Rt
738		Same as before
737	6.0 5.0 3.2 4.8 3.6 69. 76. 96. 102. 107.	5.0 3.8 4.5 3.7 136. 157. 177 183
736	5.2 6.0 3.5 2.8 2.6 62 71. 75. 100. 114.	3.6 2.8 3.7 3.6 136 179 181. 183.
735	6.5 6.2 4.5 2.9 2.7 56. 62. 67. 81. 100.	2.4 2.1 2.7 2.9 3.5 124. 150. 176. 180 183.
734	7.3 4.6 3.6 2.5 2.9 61. 68. 81. 100. 130.	2.3 2.5 3.1 3.0 3.3 153. 178. 180. 183. 187.
733	8.3 7.8 7.4 5.2 4.8 43. 55 60. 66. 83.	4.4 3.1 3.6 2.7 3.1 4.0 100. 125. 156. 182 188 189.
732	7.2 7.9 5.6 4.4 4.9 48. 60. 66. 82. 125.	4.6 3.9 5.6 155. 187. 188.
731	7.9 8.4 4.9 4.5 4.7 47. 58. 65. 82. 100.	4.6 4.0 5.0 130. 183. 185.
730	8.7 8.5 8.5 5.2 5.5 49. 56 58. 63. 72.	3.7 4.0 4.8 5.8 83. 116. 181. 183.
729	7.8 7.5 3.9 3.0 3.2 51. 61. 65. 84. 128.	3.3 4.6 6.4 7.2 160. 178. 180 182.
728	7.6 3.9 3.1 2.6 60. 65. 100. 123.	4.2 4.6 5.8 154. 179. 181.
727	8.0 2.9 3.5 3.0 63. 70. 94. 123.	3.3 3.7 5.2 157. 176 178.
726	8.1 7.9 5.0 3.7 4.1 50. 59. 66. 73. 100.	4.8 3.3 4.3 3.9 130. 161. 164. 167.
725 Same as before		

1694

opp. 24" Pipe Simmon's Back Levee. Grade 0.5
" H 740+03.8.
West End of Pipe Elev. bott: 4.5
East " " 4.0

Sta		Grade for Bott: Pipe	L	C	R
	3/4-1 Slope	5' wide in bottom			
0+00	West End Pipe	4.5	0.0 2.5	0.0	0.0 2.5
0+15		4.4	+5.5 6.6	+5.5	+5.5 6.6
0+30		4.3	+10.2 10.1	+10.2	+10.2 10.1
0+45		4.2	+7.6 8.2	+7.6	+7.4 8.1
0+60		4.1	+5.0 6.2	+4.7	+4.4 5.8
0+75		4.0	0.0 2.5	0.0	0.0 2.5

Part of Excavation above replaced from Borrow Pit (Force Work)

Sta	L	C	R
0	0.0 8.0	0.0	0.0 8.0
+22.5	+6.0 8.0	+6.0	+6.0 8.0
+45	0.0 8.0	0.0	0.0 8.0

Note. These Quantities to be deducted from Millard's Final Est: as it was replaced Force Work.
A.G.S.

Pages 47 ~~To~~ Used In
Final Estimate No. 2/7

X Sections of Simmons Back Levee

Sta.	Grade	Levee 8' wide 3-1 slope on Left (East 2½-1 " " Rt (West
0 = 4740+03.8	19.00	
0+20		0.0 0.0 0.0 4.0 4.0
0+50		-13.5 -8.6 -4.0 -3.1 -3.1 -3.4 -5.5 -13.4 -14.4 44.5 30 18. 4 4. 12. 26 40.0
0+75		-5.0 -3.8 -3.4 -3.7 -7.1 19.0 4 4 21.8
1		-10.0 -7.3 -3.4 -3.1 -3.1 -4.6 -12.0 -12.9 34.0 19. 4. 4. 10. 25. 32.9
1+50		-10.0 -9.3 -4.5 -4.4 -4.4 -10.6 34.0 28. 4. 4.0 30.9
2+00		-13.0 -5.0 -4.3 -4.8 -14.5 43.0 4. 4. 40.2
2+40		-15.2 -5.2 -4.5 -5.0 -15.8 -15.6 42.0 4. 4. 36. 43.0
2+50		0.0 0.0 0.0 4.0 4.0

#403-50 L.

Exc. out of Borrow Pit
for Pipe filling Feb 17/10